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(54) Title: SPHERONISED SELF-EMULSIFYING SYSTEM FOR HYDROPHOBIC AND WATER-SENSITIVE AGENTS		
(57) Abstract <p>A self-emulsifying system which comprises: I) a first portion comprising microcrystalline cellulose; and II) a second portion comprising: (A) up to 200 %, based on the weight of the first portion, of an oily substance; (B) between 2 and 100 %, based on the weight of the first portion, of a surfactant; and (C) between 2 and 1000 %, based on the weight of the oily substance and the surfactants, of water; wherein the total weight of the oily substance and the surfactant is between 2 and 200 % of the first portion, is disclosed, which is particularly useful for providing solid dosage forms of hydrophobic or water sensitive agents when dried or extruded and spheronised.</p>		

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SPHERONISED SELF-EMULSIFYING SYSTEM
FOR HYDROPHOBIC AND WATER-SENSITIVE AGENTS

The present invention relates to mixtures suitable for formulating
5 hydrophobic and water-sensitive active agents, these mixtures when dried,
processes for producing dosage forms from the mixtures in the wet or dry
states and the dosage forms themselves.

Self-emulsifying drug delivery systems have been shown to be a
method of increasing the bioavailability of poorly water soluble active
10 agents, such as drugs, and are an alternative to traditional formulations of
lipophilic active agents.

A self-emulsifying system is a mixture of oil and surfactant which
forms a fine oil-in-water emulsion when introduced into an aqueous phase
under conditions of gentle agitation. Such mixtures can be used as, for
15 example, pharmaceutical oral drug delivery systems for lipophilic
compounds by dissolving the drug in the oil phase. The system is expected
to self-emulsify rapidly in the aqueous contents of the stomach, thereby
presenting the drug in solution in small droplets of oil. The gentle
agitation required for the emulsification is provided by the digestive
20 motility of the stomach. Fine oil droplets should empty rapidly from the
stomach and promote wide distribution of the drug throughout the
gastrointestinal tract, thereby minimising irritation frequently
encountered with extended contact between bulk drug substances and the
gut wall. The self-emulsifying drug delivery systems also provide a large
25 interfacial area across which the drug can diffuse into the gastrointestinal
fluids. Since the drug is dissolved in the oil phase the dissolution step,
which can be absorption rate limiting for poorly water soluble drugs, is
eliminated.

Several combinations of oil and surfactant have been used to
30 produce self-emulsifying systems. The ingredients most frequently used
are medium chain triglyceride oils (vegetable oils) and nonionic

surfactants, which are acceptable for oral ingestion. Factors affecting the efficiency of a self-emulsifying system are the HLB and concentration of the surfactant. The dosage forms which result from these systems are usually either liquids or hard or soft gelatin capsules.

5 However, such liquid formulations are unpalatable and inconvenient to use. Hard gelatin capsules suffer leakage and soft gelatin capsules often require expensive contract formulation and manufacture. It would be advantageous to provide a self-emulsifying system for the delivery of an active agent, including but not limited to a pharmaceutical,
10 as a solid dosage form. Hitherto, such a formulation has not been satisfactorily achieved. Surprisingly, the present invention provides a self-emulsifying system suitable for solid formulation.

The present invention provides a self-emulsifying system which comprises:

- 15 I. a first portion comprising microcrystalline cellulose; and
 II. a second portion comprising:
 (A) up to 200%, based on the weight of the first portion, of an oily substance;
 (B) between 2 and 100%, based on the weight of the first
20 portion, of a surfactant; and
 (C) between 2 and 1000%, based on the weight of the oily substance and the surfactants, of water;

wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion.

25 Microcrystalline cellulose is commercially available, for example under the name Avicel®. The term includes, but is not limited to, pharmaceutical grade microcrystalline cellulose as defined in the British Pharmacopeia. Various grades of microcrystalline cellulose are described in the Handbook of Pharmaceutical Excipients, 2^e, ed. by Wade and
30 Weller, 1994, London and Washington, pages 84 to 87. As an alternative to microcrystalline cellulose powdered cellulose may be used.

Again, the powdered cellulose may be, but is not limited to, pharmaceutical grade. A description of various grades can be found in the above reference at pages 88-90.

5 The oily substance generally comprises a fatty acid ester or a long chain saturated, partially unsaturated or unsaturated long chain hydrocarbon. Thus the oily substance is preferably a C_{1-20} ester of a C_{6-30} acid or a C_{20-100} hydrocarbon or a mixture thereof.

10 The C_{6-30} acid may be naturally occurring or synthetic and generally contains one, two, three, four or more double bonds, particularly one, two or three double bonds, and may be substituted with one or more hydroxy groups. The C_{1-20} ester is the residue of a C_{1-20} alcohol comprising one, two or three hydroxy groups, which alcohol may be naturally occurring or synthetic. The acid and ester are generally linear or branched but may contain cyclic portions.

15 The C_{20-100} hydrocarbon is unsaturated, partially saturated or saturated, and is preferably saturated. It may be linear or branched or contain cyclic portions but is preferably linear. It preferably contains 30-80 carbon atoms.

20 Examples of fatty acids include, but are not limited to, caproic acid, capric acid, caprylic acid, oleic acid, palmoic acid, stearic acid, linoleic acid, octanoic acid, decanoic acid, linolenic acid, palmitic acid, palmitoleic acid, arachidic acid, myristic acid, behenic acid and lignic acid. Mono, di and tri glycerides of these fatty acids are favoured, in particular medium chain mono and diglycerides. Capric acid and caprylic acid are favoured.

25 Naturally occurring vegetable oils such as soyabean oil may be used.

Examples of C_{20-100} hydrocarbon are various grades of paraffin.

The surfactant may be any known surfactant which reduces the surface tension of the water or the oily substance thus facilitating mixing. The surfactant may be cationic, anionic, non-ionic or amphoteric. A particularly favoured surfactant is polysorbate 80, generally used at 15 -

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50% w/w. A mixture of surfactants may be used such as polysorbate 80 and span 80. Span 80 is generally used at 5 – 25% w/w.

The amount of oily substance present is preferably up to 90%, particularly between 5 and 80%, more particularly between 10 and 50%,
5 especially between 20 and 42% of the weight of the first portion.

The amount of surfactant present is preferably between 10 and 90%, particularly between 20 and 80%, and more particularly between 20 and 50% of the weight of the first portion.

The amount of water present is preferably between 2 and 150%,
10 more preferably between 2 and 100%, particularly between 3 and 80%, more particularly between 5 and 60% and especially between 8 and 42% of the weight of oil and surfactant.

The combined weight of the second portion is preferably between 30 and 95% and particularly between 35 and 95% by weight of the first
15 portion and especially between 40 and 90%.

The precise quantities of surfactant, oily substance and water which may be present will depend on the particular nature of these substances.

Specific combinations of oil and surfactant that may be used are:
mono and diglycerides USNF (50% w/w) and polysorbate 80 NF (50% w/w);
20 mono and diglycerides USNF (70% w/w), polysorbate 80 NF (20% w/w) and span 80 (10% w/w); and soyabean oil (30%) w/w, polysorbate 80 NF (49% w/w) and span 80 (21% w/w).

The optimal quantities for forming a dosage form, or for making a mixture suitable for extrusion and spheronisation can easily be
25 determined by trial and error using standard equipment. For example if spheronised pellets are desired the mixture will be too wet if an agglomerate is obtained and will be too dry if the particles disintegrate during spheronisation. Nevertheless wetter or drier mixtures may be suitable for drying to powders which may be used for filling or tableting
30 to produce dosage forms.

In a preferred embodiment the self-emulsifying system further comprises an active agent. The active agent may be, but is not limited to, a pharmaceutical, veterinary product, agrochemical, pesticide, dye or radiochemical. In particular, it is envisaged that the self-emulsifying system may be used to carry any hydrophobic or water sensitive active agent.

In a further embodiment the first portion further comprises a filler. The filler may be any conventional filling material used in various branches of formulation technology, such as lactose or another sugar. Other common fillers are calcium carbonate and glyceryl monostearate. The filler may be present in an amount of 0 to 75% based on the weight of the microcrystalline cellulose, particularly 0 to 50%.

In particular the present invention is surprisingly useful for providing solid dosage forms of hydrophobic or water sensitive active agents.

Accordingly the present invention comprises a mixture comprising:

- I. a first portion comprising microcrystalline cellulose and optionally a filler; and
- II. a second portion comprising:
 - (A) up to 200%, based on the weight of the first portion, of an oily substance;
 - (B) between 2 and 100%, based on the weight of the first portion, of a surfactant;
 - (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and
 - (D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;

wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; which mixture is dried.

The active ingredient is preferably present in an amount of between 0.5 and 50%, particularly between 2 and 40%, more particularly between 5 and 25%, based on the weight of the oily substance and surfactant.

The mixture is generally dried at about room temperature to about 5 60°C, depending on the nature of the mixture. The drying should be done below a temperature causing degradation of any of the components. Drying is generally carried out until the mixture loses no more water or at least until the mixture is sufficiently dry to process into a solid dosage form. Drying may be carried out on a tray in an oven or by fluidised-bed 10 drying or other conventional methods.

This drying step may be carried out before or after further processing of the mixture. If carried out before processing the dry mixture may be compressed into tablets or used to fill dosage forms.

Alternatively, before drying the mixture may be extruded by 15 conventional means, for example through a 1mm die. The extrudate may then be dried and compressed into tablets, or spheronised by conventional means before drying with the resulting pellets optionally being compressed into tablets.

The present invention therefore provides a solid dosage form 20 obtainable by drying a mixture comprising:

I. a first portion comprising microcrystalline cellulose and optionally a filler; and

II. a second portion comprising:

(A) up to 200%, based on the weight of the first portion, of 25 an oily substance;

(B) between 2 and 100%, based on the weight of the first portion, of a surfactant;

(C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and

30 (D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;

wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion.

In particular the dosage form is a tablet or filled capsule. The filled capsule may be made of soft or hard gelatin, particularly hard gelatin.

5 Thus the present invention provides a process for making a solid dosage form comprising drying a mixture comprising:

I. a first portion comprising microcrystalline cellulose and optionally a filler; and

II. a second portion comprising:

10 (A) up to 200%, based on the weight of the first portion, of an oily substance;

(B) between 2 and 100%, based on the weight of the first portion, of a surfactant;

15 (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and

(D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;

20 wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; and compressing the dried mixture into a tablet.

There is also provided a process for making a solid dosage form comprising extruding and spheronising a mixture comprising:

I. a first portion comprising microcrystalline cellulose and optionally a filler; and

25 II. a second portion comprising:

(A) up to 200%, based on the weight of the first portion, of an oily substance;

(B) between 2 and 100%, based on the weight of the first portion, of a surfactant;

30 (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and

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(D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;

wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; drying the spheronised pellets
5 and either filling a capsule with the pellets or compressing the pellets into a tablet.

The same preferred features given above for the mixtures apply to the solid dosage forms also.

The term "spheronised" is intended to refer to pellets which have
10 been processed on spheronisers used in the field of formulation, whether if a suitable size for laboratory or industrial scale processing, or prepared on other devices giving equivalent pellets. Such spheronisers are run at conventional speeds.

Further advantages of the present invention are that the mixture
15 can be extruded at higher pressures than normally possible without clogging or disintegration. Further, the extrudate readily forms spheronised pellets even if the extrudate is prone to initial disintegration. Also the nature of the spheronised pellets is not affected by excess time on the spheroniser after they are formed. Thus the mixture shows excellent
20 handling properties and stability during processing. The dried mixture also demonstrates good stability. In addition the mixtures of the present invention may comprise surprisingly large amounts of oily substance upon addition of a small quantity of water to the wet mixture.

It is understood that self-emulsifying systems other than mono and
25 diglycerides with polysorbate 80 may be used in the present invention, such as those disclosed in WO-A-9119563.

The following Example illustrates the present invention.

EXAMPLE

Microcrystalline cellulose (Avicel® PH 101) (FMC International, Little Island, Cork, Ireland) and lactose (Pharmatose® 200M) (DMV International, Vehgel, The Netherlands) was used as filling and pellet
5 forming material. MP (Mono- and diglycerides USNF (50% w/w) / Polysorbate 80 USNF 50% w/w). Deionized water (W) was used for preparation of MPW.

The experimental design employed in this study was a central composite design with two independent factors and five levels of each
10 factor. This gave a total of 13 experiments, including the centre point and four interaction points (Podczek, 1996). The independent factors were chosen to be the ratio of lactose to Avicel® and the ratio of MP to water. The responses to be studied were MPW and MP content of the powder mass; extrusion force; median size, size spread, disintegration time, tensile
15 strength, surface roughness and shape of the pellets. The amount of MPW required for each batch was not known and had to be assessed by trial and error. Preliminary experiments were performed to set the limits of the levels of the independent factors. For the composition of the 13
formulations, (Table 1: Quantities of liquid incorporated and the steady
20 state extrusion force). The formulations were produced in random order.

The results were analysed with univariate analysis of variance (ANOVA) to allow identification of statistically significant correlations between the independent factors and the responses, using SPSS 8.0 for Windows (Podczek, 1996).

25 MPW mixtures were prepared by adding the MP to the water and stirring with a magnetic stirrer for 10 minutes. The mixtures were used on the same day as they were prepared.

Avicel® and lactose (50g total) were pre-blended with a pestle and mortar and wetted by gradual addition of MPW. Extrusion was carried
30 out with a ram extruder (Lloyd MX50) with a die of 1mm in diameter and 6mm in length, extrusion speed 200mm/minute. A force/displacement

curve was obtained for each extrusion to allow determination of the extrusion force. The extrudate was spheronized for 10 minutes on a 120mm diameter spheronizer (Caleva) using a cross-hatch friction plate with speed of 1880 rpm. The resulting pellets were dried in an oven at
5 40°C until they reached constant weight.

Size analysis was performed using a nest of British standard sieves (500, 710, 1000, 1400, 2000, 2800, 4000 and 5600 µm aperture) agitated on a sieve shaker for 10 minutes. Retained weight data were used to construct cumulative % undersize distributions. Median diameter and
10 spread was determined as the 50% value and the difference between 99% and 1%.

The disintegration of the pellets was studied in deionized water at 37°C using a disintegration apparatus (BP 1998, modified with a 1mm mesh at the base of the tubes). Six pellets from each batch were tested.
15 The end point was taken as the time for disruption of the pellets.

The crushing strength of the pellets was analysed using a CT5 tester (Engineering Systems, Nottingham, UK) with a 5 kg load cell and a speed of 1.0mm/minute. A random sample of 10 pellets was tested. The crushing load was converted into surface tensile stress using the following
20 equation (Shipway and Hutchings. 1993):

$$\sigma_f = (0.4F_0)/(\pi R^2)$$

where σ_f is the surface tensile stress [N/m²], F is the crushing load [N] and R is the radius [m]. The radius was calculated from the Feret diameter.

The shape of the pellets was studied by image analysis using a
25 Seescan Image Analyser (Seescan, Cambridge, UK), completed with a black and white camera (CCD-4 miniature video camera module, Rengo Co. Ltd. Toyohashi, Japan) connected to a zoom lens (18-108/2.5, Olympus, Hamburg, Germany). A shape factor, to describe the roundness of the pellets, and the Feret diameter was determined by analysing a random
30 sample of 100 pellets from each batch. (Podczek and Newton, 1994: Podczek and Newton, 1995).

The surface roughness of the pellets was studied using a non-contacting laser profilometer (UBM Microfocus Measurement System, UBM Messtechnik GmbH, Ettlingen, Germany) with a light spot diameter of $1\mu\text{m}$ and a measurement range of $\pm 500\mu\text{m}$. The area scanned was
5 $0.3 \times 0.3\text{mm}$ with a resolution of 1000 points/mm in both directions. Scans were levelled to remove any underlying slope or curvature. The UBSOFT (UBM Messtechnik GmbH, Ettlingen, Germany) associated with the laser profilometer system was used to determine four different roughness parameters: R_a , R_q , R_{tm} and fractal dimension (Podczek, 1998). Five
10 pellets from each batch was studied.

The amount of MPW required for each formulation was not known and had to be assessed by trial and error until a 'good' product without any apparent agglomerates was formed. If the formulation gave agglomerates the amount of MPW was lowered. Some formulations gave a good product
15 on the first attempt. In total 25 batches were produced (Table 1). After sieving the 'best' batch from each formulation was chosen for further analysis. Batches with pellets larger than $2800\mu\text{m}$ were excluded (Table 2: Retained weight (g) of pellets in the size fractions).

According to the model equation and assuming that all the water
20 evaporated, the maximum amount of MP that could be incorporated was 36g (MP:water ratio 92:8, lactose:Avicel® ratio 0:100), which is 42% of dry pellet weight.

Statistical analysis of the extrusion forces showed a linear relationship with the MP:water ratio, the more MP the higher extrusion
25 force. The lactose:Avicel® ratio had no statistically significant influence. As for the spheronization process formulation number 9 seemed to have a different mechanism of spheronization than what has been proposed (Chapman, 1985). The extrudate first broke into powder and pellets started to form after a few minutes. With many of the formulations some
30 powder was stuck on the plate after the spheronization. This can be a

problem in pharmaceutical production when batch after batch is loaded onto the spheronizer.

Both parameters describing the pellet size distribution, median diameter and size spread, were found to be dependent on the MP:water ratio (Table 3: Results of the size analysis). The median diameter increases with increased amount of MP and levels off. The size spread has a linear relationship with the MP:water ratio and increases with increased amount of MP. No statistically significant correlation with the lactose:Avicel® ratio could be found.

Statistical analysis of the disintegration results showed a cubic correlation between disintegration time and MP:water ratio in size fraction 1000-1400 µm, values are mean for 6 pellets (Table 4). The disintegration time increases dramatically when the water content is increased from 70% to 100%. The lactose:Avicel® ratio had no statistically significant influence (Table 5: Crushing load on pellets in size fractions 710-1000 µm and 1000-1400 µm, values are mean of 10 pellets).

The surface tensile stress was studied in two size fractions. Statistical analysis of the results showed a quadratic relationship between tensile stress and the MP:water ratio for both size fractions. The lactose:Avicel® ratio had a small influence on the tensile stress in size fraction 710-1000µm but no effect in size fraction 1000-1400µm. Reasons for this difference could be that the pellets are formed in different ways or have a different composition, which could affect the mechanical properties. Some of the pellets, those with a MP content of 60% or more, did not snap, but were squashed between the platens. They deformed plastically, yet there was a yield load.

Statistical analysis of the shape factor showed that there was no statistically significant correlation with either of the two independent factors (Table 6: shape factors (Ecc) for the pellets in size fractions 710-1000 µm and 1000-1400 µm. Values are mean of 100 pellets). This means

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that there is no systematic change in shape as the independent factors are varied.

The surface roughness is presented as maximum peak to valley height for size fraction 1000-1400 μm (Table 7). Rtm. Oneway ANOVA
5 showed that this parameter would be best to describe the surface roughness. Statistical analysis showed that Rtm was dependent on both the MP:water ratio and the lactose:Avicel® ratio. The roughness has a minimum and according to the model equation the smoothest pellets would be made of 100% Avicel® and MPW with 59% MP.

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CLAIMS

1. A self-emulsifying system which comprises:
 - I. a first portion comprising microcrystalline cellulose; and
 - 5 II. a second portion comprising:
 - (A) up to 200%, based on the weight of the first portion, of an oily substance;
 - (B) between 2 and 100%, based on the weight of the first portion, of a surfactant; and
 - 10 (C) between 2 and 1000%, based on the weight of the oily substance and the surfactants, of water;wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion.
- 15 2. A self-emulsifying system according to claim 1 wherein the amount of oily substance present is between 20 and 42% of the weight of the first portion.
3. A self-emulsifying system according to claim 1 or 2 wherein the
20 amount of surfactant present is between 20 and 50% of the weight of the first portion.
4. A self-emulsifying system according to claim 1, 2 or 3 wherein the
amount of water present is between 8 and 42% of the weight of oil
25 and surfactant.
5. A self-emulsifying system according to any preceding claim wherein
the combined weight of the second portion is between 40 and 90% by
weight of the first portion.

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6. A self-emulsifying system according to any preceding claim which further comprises between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient optionally chosen from a pharmaceutical, veterinary product, agrochemical, pesticide, dye and a radiochemical.
7. A self-emulsifying system according to any preceding claim wherein the first portion further comprises a filler in an amount of 0 to 75% based on the weight of the microcrystalline cellulose.
8. A self-emulsifying system according to any preceding claim wherein the surfactant is polysorbate 80 or a mixture thereof with span 80.
9. A self-emulsifying system according to any of claims 1 to 7 wherein the combination of oily substance and surfactant is mono and diglycerides USNF (50% w/w) and polysorbate 80 NF (50% w/w); mono and diglycerides USNF (70% w/w), polysorbate 80 NF (20% w/w) and span 80 (10% w/w); or soyabean oil (30%) w/w, polysorbate 80 NF (49% w/w) and span 80 (21% w/w).
10. A mixture comprising:
- I. a first portion comprising microcrystalline cellulose and optionally a filler; and
- II. a second portion comprising:
- (A) up to 200%, based on the weight of the first portion, of an oily substance;
- (B) between 2 and 100%, based on the weight of the first portion, of a surfactant;
- (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and

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(D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient; wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; which mixture is dried.

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11. The mixture of claim 10 wherein the active ingredient is present in an amount of between 5 and 25% based on the weight of the oily substance and surfactant.

10 12. A solid dosage form obtainable by drying a mixture comprising:
I. a first portion comprising microcrystalline cellulose and optionally a filler; and
II. a second portion comprising:
15 (A) up to 200%, based on the weight of the first portion, of an oily substance;
(B) between 2 and 100%, based on the weight of the first portion, of a surfactant;
(C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and
20 (D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;
wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion.

25 13. A process for making a solid dosage form comprising drying a mixture comprising:
I. a first portion comprising microcrystalline cellulose and optionally a filler; and
II. a second portion comprising:
30 (A) up to 200%, based on the weight of the first portion, of an oily substance;

- (B) between 2 and 100%, based on the weight of the first portion, of a surfactant;
- (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and
- 5 (D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;
- wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; and compressing the dried mixture into a tablet.
- 10
14. A process for making a solid dosage form comprising extruding and spheronising a mixture comprising:
- I. a first portion comprising microcrystalline cellulose and optionally a filler; and
- 15 II. a second portion comprising:
- (A) up to 200%, based on the weight of the first portion, of an oily substance;
- (B) between 2 and 100%, based on the weight of the first portion, of a surfactant;
- 20 (C) between 2 and 1000%, based on the weight of the oily substance and the surfactant, of water; and
- (D) between 0.1 and 100%, based on the weight of the oily substance and the surfactant, of an active ingredient;
- wherein the total weight of the oily substance and the surfactant is between 2 and 200% of the first portion; drying the spheronised pellets and either filling a capsule with the pellets or compressing the pellets into a tablet.
- 25

Table 1.

Formulation number*	lactose: Avicel (%)	MP: water (%)	Mass of MPW (g)	Mass of MP (g)	Extrusion force (kN)
1.1	0:100	46:54	39.962	18.38	13.6
2.1	12.75:87.5	46:54	42.980	19.77	6.7
2.2	12.75:87.5	46:54	40.923	18.83	8.0
2.3	12.75:87.5	46:54	37.983	17.47	11.3
3G.1	25:75	46:54	33.036	15.20	12.9
4.1	37.5:62.5	46:54	32.976	15.17	8.9
4.2	37.5:62.5	46:54	29.962	13.78	12.9
5.1	50:50	46:54	27.810	12.79	10.2
5.2	50:50	46:54	26.777	12.32	11.7
6.1	25:75	0:100	42.992	0	4.6
6.2	25:75	0:100	40.012	0	6.3
6.3	25:75	0:100	38.016	0	9.3
6.4	25:75	0:100	36.050	0	10.7
7.1	25:75	23:77	37.987	8.74	8.7
8.1	25:75	69:31	31.916	22.02	13.7
9.1	25:75	92:8	30.746	28.29	17.8
9.2	25:75	92:8	33.527	30.85	14.8
10i.1	5:95	12:88	51.324	6.16	5.6
10i.2	5:95	12:88	48.960	5.88	6.4
10i.3	5:95	12:88	47.238	5.67	7.8
10i.4	5:95	12:88	44.104	5.29	11.1
11i.1	5:95	80:20	38.986	31.19	11.8
12i.1	45:55	12:88	30.133	3.62	9.7
12i.2	45:55	12:88	31.987	3.84	7.1
13i.1	45:55	80:20	27.128	21.70	16.4

*Batches chosen for analysis in bold.

Table 2.

Formulation number*	Size fractions (µm)											
	<500	500-710	710-1000	1000-1400	1400-2000	2000-2800	2800-4000	4000-5600	>5600			
1.1	0	0.020	0.181	16.992	27.478	0.005	0	0	0			
2.1	0	0.012	0.052	0.386	3.711	9.441	11.248	9.521	10.410			
2.2	0.041	0.060	0.205	7.132	16.710	10.172	3.155	1.159	6.598			
2.3	0	0.016	0.440	24.039	20.439	0.023	0	0	0			
3G.1	0	0.045	0.433	22.408	22.537	0	0	0	0			
4.1	0.086	0.155	0.338	4.665	14.468	11.730	5.840	2.656	8.379			
4.2	0	0.090	0.738	26.228	19.928	0.033	0	0	0			
5.1	0	0	0.298	25.385	21.474	0.167	0.033	0.112	0			
5.2	0	0.038	0.611	27.400	19.185	0.074	0	0	0			
6.1	0.009	0.008	0.003	0.010	0.094	11.515	22.368	0.970	0			
6.2	0.049	0.030	0.066	2.345	13.989	8.550	1.872	2.709	0.690			
6.3	0.347	4.058	23.889	5.518	0.692	0.497	0	0	0			
6.4	0.390	6.532	22.499	1.593	0.061	0	0	0	0			
7.1	0	0.051	1.993	36.090	1.169	0.008	0	0	0			
8.1	0.024	0.035	0.338	22.389	29.592	0.034	0	0	0			
9.1	0.669	1.969	8.154	19.651	7.220	4.229	0	0	0			
9.2	0.080	0.021	0.099	8.918	31.377	7.248	0	0	0			
10i.1	0.005	0.007	0.016	1.108	12.766	16.106	3.094	0	0			
10i.2	0.079	0.132	0.492	3.570	11.806	10.091	2.487	2.394	2.129			
10i.3	0.249	0.812	5.575	10.972	6.828	1.503	0.854	3.885	2.328			
10i.4	0.324	3.365	24.118	5.977	0.006	0	0	0	0			
11i.1	0.036	0.026	0.343	21.784	26.767	0.015	0	0	0			
12i.1	0.030	1.128	21.061	17.296	0.162	0	0	0	0			
12i.2	0.113	0.286	1.711	14.675	15.737	3.159	1.069	2.144	0			
13i.1	0.128	0.053	4.448	7.079	33.085	6.510	0	0	0			

* Batches chosen for analysis in bold.

Table 3.

Formulation number	median diameter (μm)	spread (μm)	size fraction mode value	% in modal fraction
1.1	1524	1000	1400-2000	61.5
2.3	1365	1290	1000-1400	53.5
3G.1	1397	1290	1400-2000	49.6
4.2	1349	1290	1000-1400	55.8
5.2	1333	1290	1000-1400	57.9
6.4	810	1050	710-1000	72.4
7.1	1190	1290	1000-1400	91.8
8.1	1460	1000	1400-2000	56.5
9.1	1206	2450	1000-1400	46.9
10i.4	857	900	710-1000	71.4
11i.1	1444	1000	1400-2000	54.7
12i.1	968	900	710-1000	53.1
13i.1	1651	2090	1400-2000	64.5

Table 4.

Formulation number	Disintegration time (min)	s.d.
1.1	8.04	1.16
2.3	4.94	0.85
3G.1	5.95	1.22
4.2	7.65	2.33
5.2	7.22	2.65
6.4	94.65	13.96
7.1	10.58	2.46
8.1	3.58	0.76
9.1	3.04	1.34
10i.4	23.82	14.38
11i.1	5.52	2.55
12i.1	15.37	3.48
13i.1	6.57	2.11

Table 5.

Formulation number	710-1000 μ m		1000-1400 μ m	
	load (kg)	s.d.	load (kg)	s.d.
1.1	0.103*	0.020	0.191	0.024
2.3	0.086	0.013	0.195	0.029
3G.1	0.092	0.010	0.193	0.014
4.2	0.072	0.012	0.166	0.027
5.2	0.075	0.011	0.152	0.019
6.4	1.723	0.228	1.888	0.939
7.1	0.236	0.067	0.492	0.085
8.1	0.027*	0.003	0.039*	0.004
9.1	0.004*	0.001	0.010*	0.003
10i.4	0.551	0.121	0.724	0.069
11i.1	0.009*	0.003	0.016*	0.003
12i.1	0.461	0.080	0.674	0.130
13i.1	0.017*	0.005	0.023*	0.006

*Deforming pellets

Table 6.

Formulation number	710-1000 μm		1000-1400 μm	
	Ecc	s.d.	Ecc	s.d.
1.1	0.5134	0.1413	0.6286	0.1027
2.3	0.5209	0.1490	0.5991	0.1047
3G.1	0.5047	0.1140	0.6253	0.1016
4.2	0.5594	0.1333	0.6052	0.1016
5.2	0.5326	0.1301	0.6054	0.09096
6.4	0.5574	0.1747	0.5141	0.1987
7.1	0.5446	0.1214	0.5892	0.1126
8.1	0.5363	0.1287	0.6219	0.08769
9.1	0.5048	0.1334	0.5296	0.1191
10i.4	0.6252	0.1101	0.6416	0.1050
11i.1	0.5238	0.1306	0.5904	0.1068
12i.1	0.5629	0.1195	0.6070	0.1222
13i.1	0.5219	0.1275	0.5438	0.1079

Table 7.

Formulation number	R _{tm} (μm)	s.d.	N
1.1	10.09	1.44	3
2.3	10.85	1.29	4
3G.1	10.86	1.30	5
4.2	13.57	1.74	4
5.2	13.36	1.67	4
6.4	14.50	0.73	3
7.1	11.47	0.63	3
8.1	9.24	1.52	4
9.1	15.36	1.19	5
10i.4	12.90	1.61	4
11i.1	8.49	0.81	5
12i.1	14.47	1.74	5
13i.1	8.73	1.35	4

N: number of observations

INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 00/00150

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 A61K9/107 A61K9/16

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 A61K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 98 32443 A (EUGSTER CONRAD HANS ;EUGSTER CARL (CH); MARIGEN SA (CH)) 30 July 1998 (1998-07-30) page 11, line 4 - line 18 page 12, line 30 -page 13, last line page 14, line 9 - line 22 page 20, line 1 -page 21, last line; claims 1,6	1-14
A	EP 0 266 323 A (KABIVITRUM AB) 4 May 1988 (1988-05-04) claims 1,2; examples 1,3,8,9	1-14

☒ Further documents are listed in the continuation of box C.

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Date of the actual completion of the international search 17 April 2000	Date of mailing of the international search report 26/04/2000
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer Marttin, E

INTERNATIONAL SEARCH REPORT

Intern nal Application No
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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>WO 97 40702 A (OLLEVIER FRANS ; ROELANTS IVO (BE); LEUVEN K U RES & DEV (BE); AGRO) 6 November 1997 (1997-11-06) page 4, line 10 - line 14 page 5, line 12 - line 36 page 7, line 11 - line 18 page 9, line 3 - line 6 page 16, line 35 - page 19, line 32; example 1 claims 22,23,36-39; example 5</p>	1-14

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/GB 00/00150

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